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**Attenuating the Luminous Output  
of the AN/PVS-5A Night Vision Goggles  
and Its Effects on Visual Acuity**

**By**

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**September 1989**

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<p>Aviators in combat may be subjected to a variety of noxious light stimuli. Filters and other eye protective devices may be used to counter these threats. At night, filters may be used in conjunction with image intensification devices (e.g., night vision goggles) to provide useful low-light vision as well as protection from deleterious light sources (e.g., lasers, pyrotechnics, nuclear fireballs, etc.). Technologies may be combined in a single, integrated head gear unit. The present study was performed in order to consider the effects on visual acuity after reducing night vision goggle luminous output from 0-99 percent. A range of target contrasts and ambient illumination levels was investigated. AN/PVS-5A goggles were selected based upon their compatibility with current phosphor display technology and their current ubiquity within aviation units. Visual acuity was assayed behaviorally because of its critical importance in flying performance. The</p> <p style="text-align: center;">(Continued) →</p>					
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results of the study provide normative acuity data with goggles alone and document the effects on goggle visual acuity with reduced goggle luminances as might be produced by protective materials placed between the goggles and the eyes.

*Keywords: light filter,  
human factors engineering, night vision devices, (RT) —*

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## Introduction

Among the threats confronting the Army aviator in combat are those that will challenge his visual integrity and impair his visual performance. Pyrotechnics, high-intensity searchlights, electronic strobes, and fireballs produced by tactical nuclear weapons all represent battlefield sources of noxious light energy with the potential to degrade visual function. A more recent threat is that of exposure to directed energy from ground- or air-based laser platforms. Such systems could be used not only to designate aircraft, but, at appropriate powers and wavelengths, to flashblind aircrews and produce ocular injury.

At present, the Army is developing an integrated flight helmet (Head Gear Unit-56/P [HGU-56/P]) that will provide visual prophylaxis against debilitating sources of light most likely to be encountered on the battlefield. One preliminary design incorporates a visor-goggle arrangement that will attenuate the exposure to both laser energy and nuclear flash. Unfortunately, along with their intended objective of providing ocular protection, protective materials placed in front of the eyes will have the additional effect of reducing the light available for seeing. (Even optical quality clear glass loses 4 percent of the incoming light per surface.) Under optimal (i.e., bright light) viewing conditions, the reduction of light due to protective devices should have but minimal effects on visual function. However, any additional loss of available light could aggravate the already limited visual capabilities of pilots at night.

One proposal offered by Army planners prescribes that pilots use image intensification ( $I^2$ ) devices (e.g., night vision goggles [NVGs]) in conjunction with the ocular protective materials to augment their nighttime viewing capabilities. While NVGs inherently compromise the quality of vision (reduced acuity, depth perception, visual field, and color vision), the operational capabilities they provide far outweigh the visual shortcomings associated with their use. However, decreasing the NVG's output brightness with filters or other protective materials could further degrade image quality and, in so doing, further impair visual function and perception. Indeed, reducing photopic acuity further could effectively hinder safe flight.

The present study was designed to examine visual acuity with AN/PVS-5 night vision goggles after reducing normal output luminance by as much as 99 percent. Data were collected in the laboratory over a range of low ambient illumination conditions and target-background contrasts. The work was conducted in

conjunction with a tasking by the Directorate of Combat Developments, U.S. Army Aviation Center, Fort Rucker, Alabama, to evaluate the effects of nuclear flashblindness material on visual acuity with NVGs (Appendix A). The data presented here extend those reported in the study performed in response to that tasking (Levine and Rash, 1989).

### Methods

Subjects: Eight volunteers, seven military and one civilian, aged from 20-37, participated in the study. All participants had 20/20 or better uncorrected Snellen visual acuity as measured under standard, clinical test conditions. Six of the eight participants had over 50 combined hours of NVG experience as subjects in prior studies and were highly familiar with the experimental procedures. The remaining two subjects were NVG-inexperienced and experimentally naive; both were permitted sufficient opportunity to practice and adapt to viewing through the goggles.

Apparatus: Subjects sat in a darkened room 20 feet from a 12" monochrome CRT upon which individual, computer-generated, Snellen letters "E" were presented as targets. Subjects viewed the CRT through a single pair of AN/PVS-5A NVGs mounted on a table in front of them (Figure 1). Goggle height and interpupillary distance were adjusted by the experimenter for each subject. Goggle batteries were changed after every 10 hours of use.

### Viewing conditions:

Background CRT luminance - Three background CRT luminances were chosen to correspond to the ambient light levels associated with twilight (1/2 hour past sunset), full moon, and starlight (clear, moonless night; RCA Electro-Optics Handbook, 1974). Light levels were simulated by using large sheets of neutral density filter material placed over the screen to achieve the required levels of "ambient" illumination. CRT brightnesses were confirmed with a Pritchard 1980-A spectrophotometer\*. The monitor served as the only source of light in the room.

Target/background contrast level - Three contrast ratios -- 90, 30, and 3 percent -- were selected to represent conditions

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\* See Appendix D



Figure 1. Subject's viewing station with mounted AN-PVS-5A night vision goggles and hand-held joystick.

of high, moderate and low target/background contrast. Following Michelson (1927), contrast was defined as:

$$\frac{\text{background luminance} - \text{target luminance}}{\text{background luminance} + \text{target luminance}}.$$

The letters always appeared darker than their surrounds (negative contrast; Figure 2).

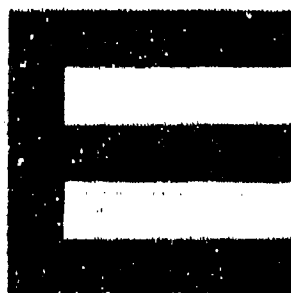
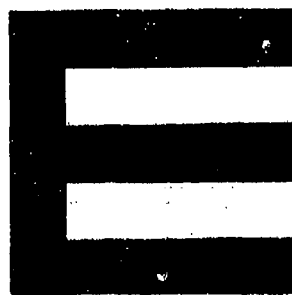


Figure 2. Snellen "E"s of high (top), medium (middle), and low (bottom) contrast.

**Goggle luminances** - The luminous output of the goggles was adjusted by a series of Kodak Wratten neutral density filters\* that were trimmed, placed in specially constructed rings, and fitted onto the oculars of the goggles (Figure 3). Optical densities and corresponding light transmittances (in parentheses) for each of the filters were as follows: 0.30 (50 percent), 0.50 (30 percent), 1.0 (10 percent), 1.5 (3 percent), and 2.0 (1 percent). In addition, a baseline no filter condition (100 percent transmission) was included in which only the empty filter rings were used. The presentation order of each of the filter conditions was determined according to a quasi-random schedule (see below).

**Procedures:** Subjects were briefed on their required tasks and permitted 5-10 minutes to adapt to their darkened surroundings. They then focused the NVGs while viewing sample targets on the monitor.



Figure 3. Night vision goggles with filters mounted onto the oculars.

During testing, the "E"s were displayed for 1 second on the CRT in one of the four cardinal orientations. The subjects indicated the orientation of the "E" with an appropriate movement of a hand-held joystick (a four-alternative forced-choice procedure). The orientation of the "E" was varied randomly under computer control while the size of the "E" and its rate of presentation (about once every 3 seconds) were controlled by an operator in an adjacent room. Letter sizes ranged, in terms of Snellen notation, from 20/10 to 20/400 (or, in terms of minimum angle of resolution, from 0.5 to 20.0 minutes of arc).

Threshold acuities were determined using the psychophysical method described by Wetherill and Levitt (1965). This technique employs a bidirectional method-of-limits to capture any one of several possible detection thresholds. A paradigm was selected to determine the 70 percent acuity threshold and modified to incorporate the four-alternative forced-choice procedure described above. The 70 percent threshold level was chosen in order to control for the effects of guessing and to provide a measure comparable to earlier work from this laboratory.

No penalties were imposed upon the subject for an incorrect or nonresponse and no performance feedback was provided. For the most difficult viewing conditions (e.g., moonlight, low contrast targets), subjects often could neither detect trial onset nor correctly identify the orientation of the largest (20/400) letter. To assist detection, subjects were cued with a verbal "ready" signal just before the start of these more "difficult" trials. (Other than providing a general orienting response, post hoc analysis indicated that this procedure had no practical consequences on the subject's performance. On "no response" trials, an acuity value of 20/600 was assigned arbitrarily and used in the calculation of the subject's threshold.)

Experimental design and data analysis. The study was conceived as a 3 (brightness: twilight, moonlight, and starlight) X 3 (contrast: high, moderate, and low) X 6 (percent goggle light transmission: 1, 3, 10, 30, 50, and 100) within-subjects design with repeated measures on all factors. Acuity, expressed in terms of the average minimum angle of resolution (MAR), served as the dependent variable. All 54 possible viewing conditions were presented randomly and exhaustively once to each subject. Data collection was accompanied over five sessions with each experimental session lasting about 1 hour.

Because NVGs deliver optimal performance (i.e., maximal brightness and peak acuity) over a limited range of ambient lighting and target conditions (clear, moonlit night, and high contrast targets), statistical analyses based upon a treatment effects model could be confounded by system limitations (producing both "ceiling" and "floor" effects). Therefore, the data are presented descriptively in order to demonstrate and clarify the functional relationships among the various levels of goggle output and their subsequent effects on visual acuity for targets of varying contrast. In addition to illustrating the effects of filters, the results also present baseline acuity data for the NVGs alone.

## Results

Acuity with NVGs alone: Table 1 presents acuities with NVGs alone ("no filter" condition) at each level of brightness and contrast. Group means and ranges are shown for each viewing condition. Acuity is represented in terms of both the minimum angle of resolution and its approximate Snellen equivalent. These data were extracted from the complete data set and are presented here to both document and provide an estimate of "best case" NVG acuity under each of the conditions tested. (Means and standard deviations also are shown graphically in Appendix B.)

As shown in Table 1, mean acuities ranged from 20/40 under the most favorable viewing conditions (twilight and high contrast) to 20/400 under the poorest (starlight and low contrast). As expected, "best" NVG acuities were achieved under system-optimal lighting conditions (twilight-moonlight) with targets of moderate to high contrast. Acuity degraded, however, with additional decreases in ambient illumination and/or contrast. At the lowest luminance and contrast level, acuity for three of the eight subjects degraded beyond measurable levels.

Table 1

Visual acuity with AN/PVS-5A night vision goggles under varying levels of brightness and contrast

	Minimum angle of resolution*		Snellen acuity**	
	Mean	Range	Mean	Range
<b><u>Twilight</u></b>				
High contrast	2.1	1.6 - 3.2	20/40	20/30-20/60
Moderate "	2.4	1.7 - 3.2	20/50	20/30-20/60
Low "	5.4	3.7 - 8.5	20/100	20/80-20/200
<b><u>Moonlight</u></b>				
High contrast	2.3	1.6 - 3.0	20/50+	20/30-20/60
Moderate "	3.5	3.0 - 4.5	20/60-	20/60-20/100
Low "	9.1	5.4 - 12.5	20/200+	20/100-20/300
<b><u>Starlight</u></b>				
High contrast	3.7	2.9 - 4.7	20/80+	20/60-20/100
Moderate "	5.7	3.9 - 7.5	20/100-	20/80-20/150
Low "	19.8	12.8 - 25.0	20/400	20/200-20/400+

\* Minutes of arc.

\*\* Approximate Snellen equivalent based upon letter sizes actually presented to the subjects.

#### Acuity with reduced NVG brightnesses:

The effects on acuity of reduced goggle output can be seen in Figures 4-6 (and in tabular form in Appendixes C-E). The data are presented as a function of percent NVG light transmission and target contrast for each level of ambient illumination. Each point represents the mean of eight subjects. Acuity is depicted both in terms of MAR and its associated Snellen equivalent. The means are plotted on log-linear axes and second order polynomial regression curves have been fitted to the data points. (Mean acuities greater than 20/400 on the graphs include the "no-response" estimates described above. In Appendixes C-E, these are depicted simply as a >20.0 MAR or as a Snellen equivalent of >20/400.)



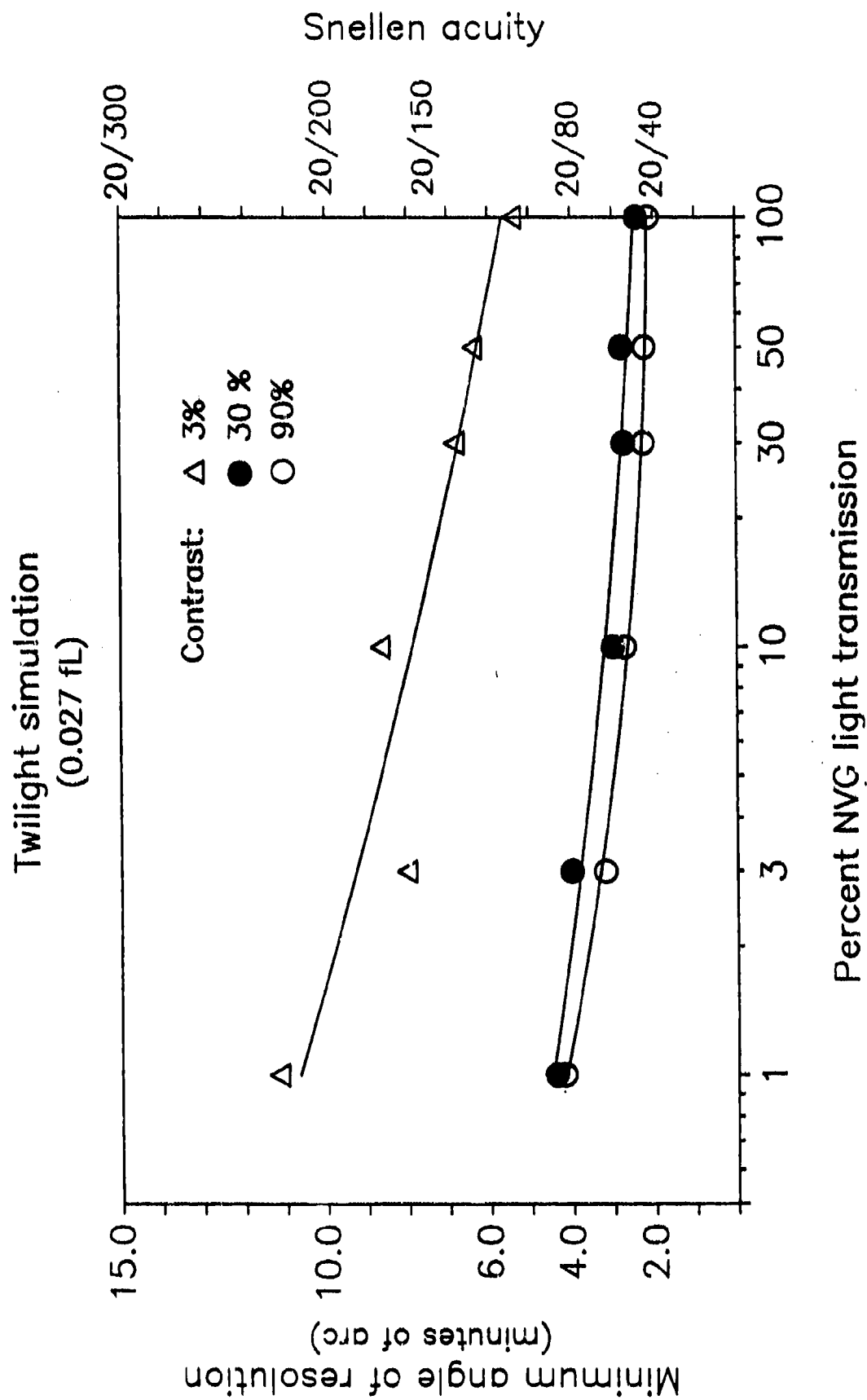
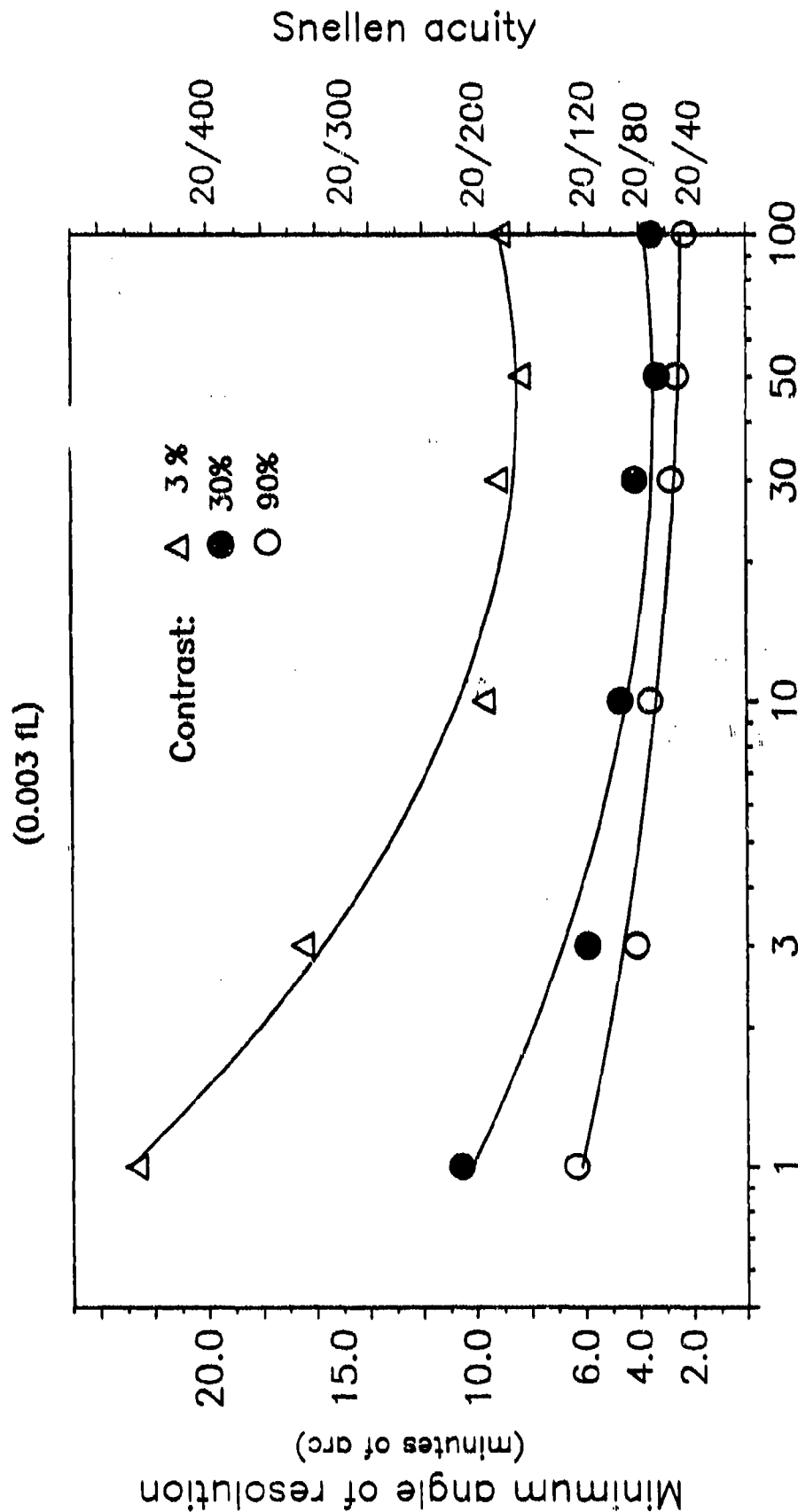


Figure 4. Visual acuity with NVGs under simulated twilight conditions: Effects of varying NVG light transmission and target contrast.

# Moonlight simulation (0.003 fL)



## Percent NVG light transmission

Figure 5. Visual acuity with NVGs under simulated moonlight conditions: Effects of varying NVG light transmission and target contrast.

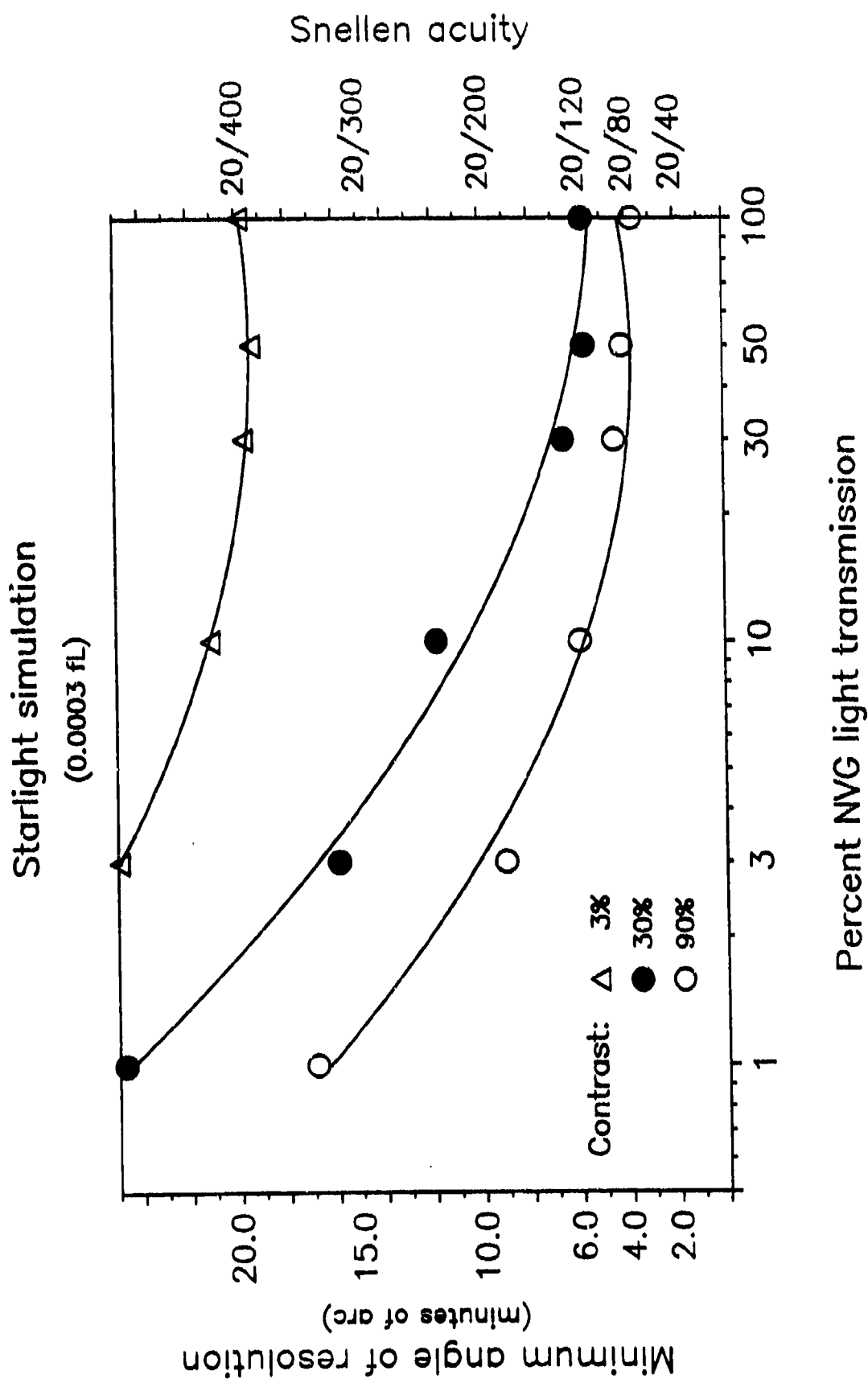


Figure 6. Visual acuity with NVGs under simulated starlight conditions: Effects of varying NVG light transmission and target contrast.

As can be seen, the specific effects of reducing goggle brightness varied as a function of both ambient light level and the target-background contrast. Under "good" NVG lighting (twilight and moonlight), acuities for medium to high contrast targets remained nearly unchanged from that of the no filter condition down to goggle brightnesses as low as 10 percent (Figures 4 and 5). At 3 percent transmittance, acuity degraded an additional 1-2 Snellen lines. At 1 percent transmittance, acuities ranged from 20/100-20/200 -- a more severe impairment. Under starlight conditions (Figure 6), acuities for both high and medium contrast targets maintained nonfilter levels down to a goggle transmittance of 30 percent. Below 30 percent transmission, acuities were more severely degraded. Acuities for low contrast targets generally were degraded under all viewing conditions, with or without filters. Under starlight conditions, acuity for targets of low contrast frequently was unmeasurable.

### Discussion and conclusions

The results of this study provide data for acuity with NVGs under both "normal" (nonfiltered) and reduced luminous output. Without filters, goggle acuity is a function of both light level and target-background contrast. Acuity is maximal for targets of medium to high contrast under moonlit conditions or better. Acuity is degraded for low contrast targets and, for all contrasts, under starlight conditions. However, as our results demonstrate, NVG output can be reduced, in some cases by an order of magnitude, without impacting visual acuity adversely.

Under both twilight and moonlight conditions, acuities for all targets (high, medium, and low contrast) remained essentially unchanged or only minimally degraded from baseline conditions with goggle transmittances as low as 10 percent. (Acuity for low contrast targets was always lower than that for medium or high.) Below 10 percent transmittance, acuity showed moderate to severe impairment. Under starlight conditions, acuity remained unchanged from baseline conditions down to 30 percent of normal transmission, although initial baseline levels were higher and losses more dramatic beyond this level.

While these data provide direction, they are far from complete parametrically. For example, the data have been obtained under benign and static conditions, and potential visual impact(s) of spectral filtration have been ignored. Modifications to goggle output ultimately will require flight testing to determine both the impact on aviator performance as well as on aviator acceptance. Until such testing is accomplished, no firm conclusions should be drawn on the operational

costs/benefits of tandem filter/NVG wear. Still, the data furnish an initial estimate of the effects of reduced goggle transmission on visual acuity and should provide a reliable baseline and a "look-up" capability with which to compare and evaluate visual performance with prototype ocular protective materials.

## References

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Appendix A

DCD request memorandum

# DISPOSITION FORM

For use of this form, see AR 340-15; the proponent agency is TAGO.

REFERENCE OR OFFICE SYMBOL	SUBJECT
ATZQ-CDM-C (70-11)	Evaluation of Visual Transmittance While Wearing Night Vision Goggles (NVG) and Nuclear Flashblindness Goggles

TO Cdr, USAARL	FROM Dir, DCD	DATE Mr. Birringer/ncw/5272	CMT 1
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1. The protection of the unaided eye against the effects of small tactical nuclear weapons (flashblindness) on the modern battlefield is an issue of concern for Army aviators. DCD is having difficulty defining the effects of reduced transmissivity of nuclear flashblindness goggles (PLZT) in terms of operational capability. This is particularly critical when aircraft are flying NOE at night and when pilots are wearing NVGs.

2. Request USAARL conduct an evaluation and analysis of the effects of visual transmittance through PLZT goggles worn in conjunction with NVGs. DCD will use this information to support or eliminate the operational capability currently required of the Aircrew Integrated Helmet (HGU-56/P). The HGU-56/P is currently in advanced development.

3. Also, request you provide a recommendation based on the analysis by 22 Nov 88.

4. DCD POC for this action is Mr. Birringer, extensions 5272/5071.

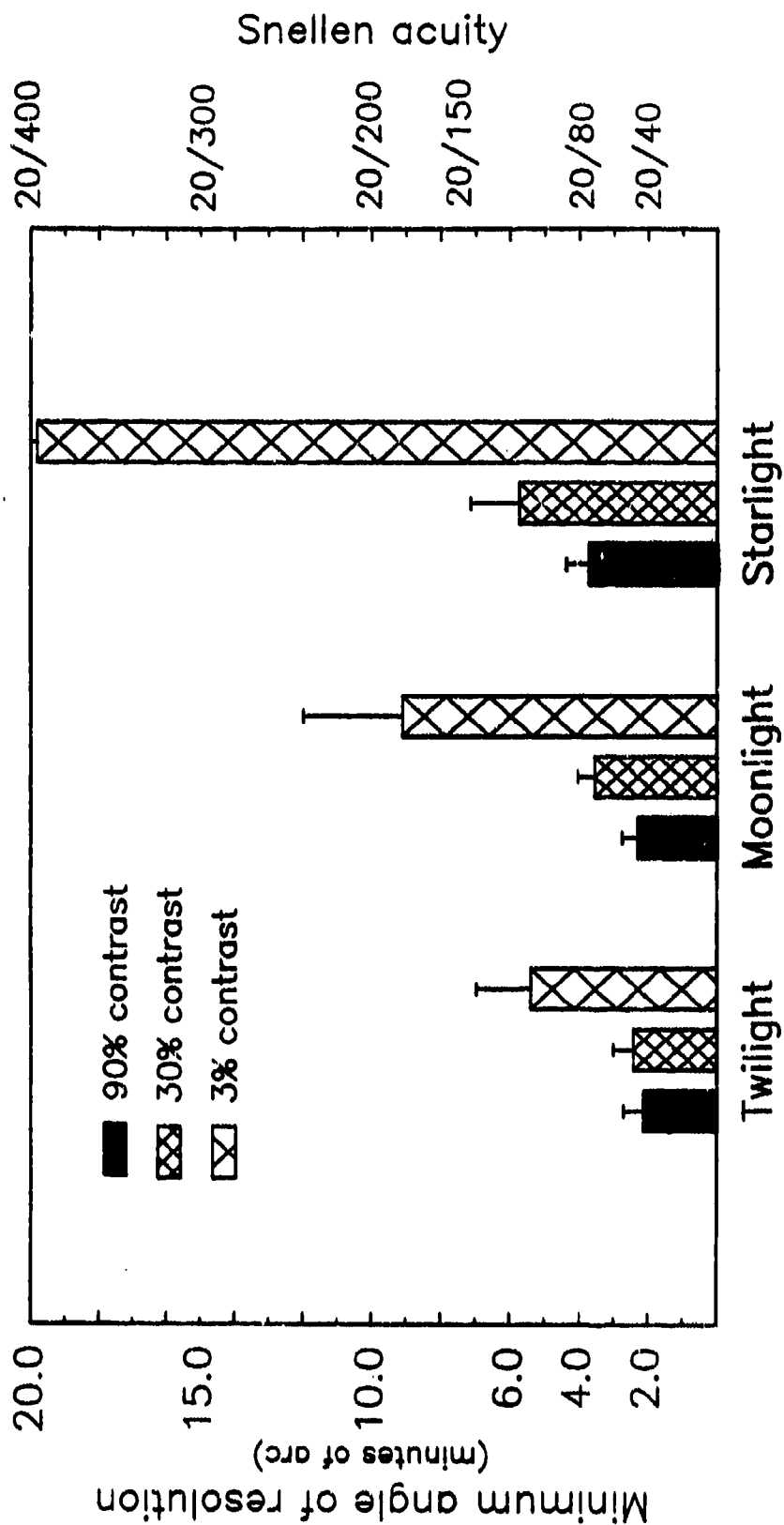
*for Theodore T. Sendak*  
THEODORE T. SENDAK  
Colonel, Aviation  
Director of Combat Developments



## Appendix B

Normal NVG acuity under varying conditions of varying light  
levels and target-background contrasts

# Normal NVG acuity



# Appendix C

Reduced NVG luminance: Acuity under "twilight" conditions

90% Contrast	Percent goggle transmission					
	100	50	30	10	3	1
Mean MAR	2.1	2.2	2.3	2.7	3.2	4.2
Range	1.6- 3.2	1.7- 3.3	1.4- 3.6	1.8- 4.4	1.8- 5.6	3.3- 5.6
Mean Snellen acuity	20/40	20/40	20/50+	20/50-	20/60	20/80
Range	20/30- 20/60	20/30- 20/60	20/30- 20/80	20/40- 20/80	20/40- 20/100	20/60- 20/100

30% Contrast						
	100	50	30	10	3	1
Mean MAR	2.4	2.8	2.8	3.0	4.0	4.4
Range	1.6- 3.2	2.0- 3.8	2.2- 3.5	2.7- 3.9	2.7- 7.5	3.0- 8.1
Mean Snellen acuity	20/50	20/60	20/60	20/60	20/80	20/80-
Range	20/30- 20/60	20/40- 20/80	20/40- 20/80	20/50- 20/80	20/50- 20/150	20/60- 20/150

3% Contrast						
	100	50	30	10	3	1
Mean MAR	5.4	6.4	6.8	8.7	8.0	11.2
Range	3.7- 8.5	5.7- 6.9	5.8- 8.5	5.0- 13.0	6.5- 10.5	7.8- 13.5
Mean Snellen acuity	20/100	20/150+	20/150	20/150-	20/150-	20/200
Range	20/80- 20/200	20/100- 20/200	20/100- 20/200	20/100- 20/300	20/150- 20/200	20/150- 20/300

# Appendix D

Reduced NVG luminance: Acuity under "moonlight" conditions

90% Contrast	Percent goggle transmission					
	100	50	30	10	3	1
Mean MAR	2.3	2.6	2.8	3.6	4.2	6.4
Range	1.6- 3.0	1.9- 3.6	1.9- 4.7	2.6- 4.2	3.3- 5.7	5.3- 8.5
Mean Snellen acuity	20/50	20/50	20/60	20/80	20/80	20/150
Range	20/30- 20/60	20/40- 20/80	20/40- 20/100	20/50- 20/80	20/60- 20/100	20/100- 20/200

30% Contrast	Percent goggle transmission					
	100	50	30	10	3	1
Mean MAR	3.5	3.3	4.2	4.7	6.0	10.6
Range	2.9- 4.5	2.5- 4.0	3.1- 7.3	3.3- 6.8	4.9- 9.8	5.8- 17.5
Mean Snellen Acuity	20/50-	20/60	20/80	20/100	20/150+	20/200
Range	20/60- 20/80	20/50- 20/80	20/60- 20/150	20/60- 20/150	20/100- 20/200	20/200- 20/400

3% Contrast	Percent goggle transmission					
	100	50	30	10	3	1
Mean MAR	9.1	8.4	9.2	9.7	16.5	>20.0
Range	5.4- 12.5	6.4- 10.8	6.2- 12.8	6.7- 12.5	9.3- >20.0	11.0- >20.0
Mean Snellen acuity	20/200+	20/150-	20/200+	20/200+	20/300	>20/400
Range	20/100- 20/300	20/150- 20/200	20/150- 20/300	20/150- 20/300	20/200- >20/400	20/200- >20/400

# Appendix E

Reduced NVG luminance: Acuity under "starlight" conditions

90% Contrast	Percent goggle transmission					
	100	50	30	10	3	1
Mean MAR	3.7	4.1	4.5	6.0	9.1	16.9
Range	2.9- 4.7	3.0- 5.8	3.4- 6.1	4.5- 11.5	5.8- 13.0	12.8- >20.0
Mean Snellen acuity	20/80+	20/80	20/100+	20/150+	20/200+	20/300
Range	20/60- 20/100	20/60- 20/100	20/60- 20/150	20/100- 20/200	20/150 20/300	20/200- >20/400

30% Contrast	100	50	30	10	3	1
	100	50	30	10	3	1
Mean MAR	5.7	5.7	6.6	11.9	15.9	>20.0
Range	4.1- 7.5	4.4- 7.5	5.1- 9.8	6.2- >20.0	12.0- >20.0	>20.0
Mean Snellen Acuity	20/100	20/100	20/150-	20/200	20/300	>20/400
Range	20/80- 20/150	20/80- 20/150	20/100 20/200	20/200- 20/400	20/200- >20/400	>20/400

3% Contrast	100	50	30	10	3	1
	100	50	30	10	3	1
Mean MAR	19.8	19.3	19.7	>20.0	>20.0	>20.0
Range	12.7- >20.0	11.3- >20.0	13.3- >20.0	10.5- >20.0	>20.0	>20.0
Mean Snellen acuity	20/400	20/400	20/400	20/400	>20/400	>20/400
Range	20/200- >20/400	20/200- >20/400	20/200- >20/400	20/200- >20/400	>20/400	>20/400

Appendix F

Manufacturers' list

Eastman Kodak Company  
Rochester, NY 14650

Photo Research  
3000 North Hollywood Way  
Burbank, CA 91505

Initial distribution

Commander  
U.S. Army Natick Research  
and Development Center  
ATTN: Documents Librarian  
Natick, MA 01760

Naval Submarine Medical  
Research Laboratory  
Medical Library, Naval Sub Base  
Box 900  
Groton, CT 05340

Commander/Director  
U.S. Army Combat Surveillance  
& Target Acquisition Lab  
ATTN: DELCS-D  
Fort Monmouth, NJ 07703-5304

Commander  
10th Medical Laboratory  
ATTN: Audiologist  
APO NEW YORK 09180

Commander  
Naval Air Development Center  
Biophysics Lab  
ATTN: G. Kydd  
Code 60B1  
Warminster, PA 18974

Naval Air Development Center  
Technical Information Division  
Technical Support Detachment  
Warminster, PA 18974

Commanding Officer  
Naval Medical Research  
and Development Command  
National Naval Medical Center  
Bethesda, MD 20014

Under Secretary of Defense  
for Research and Engineering  
ATTN: Military Assistant  
for Medical and Life Sciences  
Washington, DC 20301

Commander  
U.S. Army Research Institute  
of Environmental Medicine  
Natick, MA 01760

U.S. Army Avionics Research  
and Development Activity  
ATTN: SAVAA-P-TP  
Fort Monmouth, NJ 07703-5401

U.S. Army Research and Development  
Support Activity  
Fort Monmouth, NJ 07703

Chief, Benet Weapons Laboratory  
LCWSL, USA ARRADCOM  
ATTN: DRDAR-LCB-TL  
Watervliet Arsenal, NY 12189

Commander  
Man-Machine Integration System  
Code 602  
Naval Air Development Center  
Warminster, PA 18974

Commander  
Naval Air Development Center  
ATTN: Code 6021 (Mr. Brindle)  
Warminster, PA 18974

Commanding Officer  
Harry G. Armstrong Aerospace  
Medical Research Laboratory  
Wright-Patterson  
Air Force Base, OH 45433

Director  
Army Audiology and Speech Center  
Walter Reed Army Medical Center  
Washington, DC 20307-5001

Director  
Walter Reed Army Institute  
of Research  
Washington, DC 20307-5100

HQ DA (DASG-PSP-0)  
5109 Leesburg Pike  
Falls Church, VA 22041-3258

Naval Research  
Laboratory Library  
Code 1433  
Washington, DC 20375

Harry Diamond Laboratories  
ATTN: Technical Infor-  
mation Branch  
2800 Powder Mill Road  
Adelphi, MD 20783-1197

U.S. Army Materiel Systems  
Analysis Agency  
ATTN: Reports Processing  
Aberdeen proving Ground  
MD 21005-5017

U.S. Army Ordnance Center  
and School Library  
Building 3071  
Aberdeen Proving Ground,  
MD 21005-5201

U.S. Army Environmental Hygiene  
Agency  
Building E2100  
Aberdeen Proving Ground,  
MD 21010

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Chemical Research  
and Development Center  
Aberdeen Proving Ground,  
MD 21010-5423

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of Dental Research  
Walter Reed Army Medical Center  
Washington, DC 20307-5300

Naval Air Systems Command  
Technical Air Library 950D  
Rm 278, Jefferson Plaza II  
Department of the Navy  
Washington, DC 20361

Naval Research Laboratory Library  
Shock and Vibration Infor-  
mation Center, Code 5804  
Washington, DC 20375

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U.S. Army Human Engineer-  
ing Laboratory  
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Aberdeen Proving Ground,  
MD 21005-5001

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U.S. Army Test  
and Evaluation Command  
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Aberdeen Proving Ground,  
MD 21005-5055

Director  
U.S. Army Ballistic  
Research Laboratory  
ATTN: DRXBR-OD-ST Tech Reports  
Aberdeen Proving Ground,  
MD 21005-5066

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U.S. Army Medical Research  
Institute of Chemical Defense  
ATTN: SGRD-UV-AO  
Aberdeen Proving Ground,  
MD 21010-5425

Commander  
U.S. Army Medical Research  
and Development Command  
ATTN: SGRD-RMS (Ms. Madigan)  
Fort Detrick, Frederick,  
MD 21701



Commander  
U.S. Army Medical Research  
Institute of Infectious Diseases  
Fort Detrick, Frederick,  
MD 21701

Director, Biological  
Sciences Division  
Office of Naval Research  
600 North Quincy Street  
Arlington, VA 22217

Commander  
U.S. Army Materiel Command  
ATTN: AMCDE-XS  
5001 Eisenhower Avenue  
Alexandria, VA 22333

Commandant  
U.S. Army Aviation  
Logistics School  
ATTN: ATSQ-TDN  
Fort Eustis, VA 23604

U.S. Army Training  
and Doctrine Command  
ATTN: ATCD-ZX  
Fort Monroe, VA 23651

Structures Laboratory Library  
USARTL-AVSCOM  
NASA Langley Research Center  
Mail Stop 266  
Hampton, VA 23665

Naval Aerospace Medical  
Institute Library  
Bldg 1953, Code 102  
Pensacola, FL 32508

Command Surgeon  
U.S. Central Command  
MacDill Air Force Base  
FL 33608

Air University Library  
(AUL/LSE)  
Maxwell AFB, AL 36112

Commander  
U.S. Army Biomedical Research  
and Development Laboratory  
ATTN: SGRD-UBZ-I  
Fort Detrick, Frederick,  
MD 21701

Defense Technical  
Information Center  
Cameron Station  
Alexandria, VA 22313

U.S. Army Foreign Science  
and Technology Center  
ATTN: MTZ  
220 7th Street, NE  
Charlottesville, VA 22901-5396

Director,  
Applied Technology Laboratory  
USARTL-AVSCOM  
ATTN: Library, Building 401  
Fort Eustis, VA 23604

U.S. Army Training  
and Doctrine Command  
ATTN: Surgeon  
Fort Monroe, VA 23651-5000

Aviation Medicine Clinic  
TMC #22, SAAF  
Fort Bragg, NC 28305

U.S. Air Force Armament  
Development and Test Center  
Eglin Air Force Base, FL 32542

U.S. Army Missile Command  
Redstone Scientific  
Information Center  
ATTN: Documents Section  
Redstone Arsenal, AL 35898-5241

U.S. Army Research and Technology  
Laboratories (AVSCOM)  
Propulsion Laboratory MS 302-2  
NASA Lewis Research Center  
Cleveland, OH 44135

AFAMRL/HEX  
Wright-Patterson AFB, OH 45433

University of Michigan  
NASA Center of Excellence  
in Man-Systems Research  
ATTN: R. G. Snyder, Director  
Ann Arbor, MI 48109

John A. Dellinger,  
Southwest Research Institute  
P. O. Box 28510  
San Antonio, TX 78284

Product Manager  
Aviation Life Support Equipment  
ATTN: AMCPM-ALSE  
4300 Goodfellow Blvd.  
St. Louis, MO 63120-1798

Commander  
U.S. Army Aviation  
Systems Command  
ATTN: AMSAV-ED  
4300 Goodfellow Blvd  
St. Louis, MO 63120

Commanding Officer  
Naval Biodynamics Laboratory  
P.O. Box 24907  
New Orleans, LA 70189

U.S. Army Field Artillery School  
ATTN: Library  
Snow Hall, Room 14  
Fort Sill, OK 73503

Commander  
U.S. Army Health Services Command  
ATTN: HSOP-SO  
Fort Sam Houston, TX 78234-6000

U.S. Air Force Institute  
of Technology (AFIT/LDEE)  
Building 640, Area B  
Wright-Patterson AFB, OH 45433

Henry L. Taylor  
Director, Institute of Aviation  
University of Illinois-  
Willard Airport  
Savoy, IL 61874

COL Craig L. Urbauer, Chief  
Office of Army Surgeon General  
National Guard Bureau  
Washington, DC 50310-2500

Commander  
U.S. Army Aviation  
Systems Command  
ATTN: SGRD-UAX-AL (MAJ Lacy)  
4300 Goodfellow Blvd., Bldg 105  
St. Louis, MO 63120

U.S. Army Aviation Systems Command  
Library and Information  
Center Branch  
ATTN: AMSAV-DIL  
4300 Goodfellow Blvd  
St. Louis, MO 63120

Federal Aviation Administration  
Civil Aeromedical Institute  
CAMI Library AAC 64D1  
P.O. Box 25082  
Oklahoma City, OK 73125

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U.S. Army Academy  
of Health Sciences  
ATTN: Library  
Fort Sam Houston, TX 78234

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U.S. Army Institute  
of Surgical Research  
ATTN: SGRD-USM (Jan Duke)  
Fort Sam Houston, TX 78234-6200

Director of Professional Services  
AFMSC/GSP  
Brooks Air Force Base, TX 78235

U.S. Army Dugway Proving Ground  
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Dugway, UT 84022

U.S. Army Yuma Proving Ground  
Technical Library  
Yuma, AZ 85364

AFFTC Technical Library  
6520 TESTG/ENXL  
Edwards Air Force Base,  
CAL 93523-5000

Commander  
Code 3431  
Naval Weapons Center  
China Lake, CA 93555

Aeromechanics Laboratory  
U.S. Army Research  
and Technical Labs  
Ames Research Center,  
M/S 215-1  
Moffett Field, CA 94035

Sixth U.S. Army  
ATTN: SMA  
Presidio of San Francisco,  
CA 94129

Commander  
U.S. Army Aeromedical Center  
Fort Rucker, AL 36362

U.S. Air Force School  
of Aerospace Medicine  
Strughold Aeromedical Library  
Documents Section, USAFSAM/TSK-4  
Brooks Air Force Base, TX 78235

Dr. Diane Damos  
Department of Human Factors  
ISSM, USC  
Los Angeles, CA 90089-0021

U.S. Army White Sands  
Missile Range  
Technical Library Division  
White Sands Missile Range,  
NM 88002

U.S. Army Aviation Engineering  
Flight Activity  
ATTN: SAVTE-M (Tech Lib)  
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Edwards Air Force Base,  
CA 93523-5000

Ms. Sandra G. Hart  
Ames Research Center  
MS 239-5  
Moffett Field, CA 94035

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of Research  
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Presidio of San Francisco,  
CA 94129

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Naval Biosciences Laboratory  
Naval Supply Center, Bldg 844  
Oakland, CA 94625

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Development Activity  
Fort Detrick, Frederick,  
MD 21701-5009

Commander, U.S. Army  
Aviation Center  
Directorate  
of Combat Developments  
Bldg 507  
Fort Rucker, AL 36362

Chief  
Army Research Institute  
Field Unit  
Fort Rucker, AL 36362

Commander  
U.S. Army Safety Center  
Fort Rucker, AL 36362

U.S. Army Aircraft Development  
Test Activity  
ATTN: STEBG-MP-QA  
Cairns AAF  
Fort Rucker, AL 36362

Commander  
U.S. Army Medical Research  
and Development Command  
ATTN: SGRD-PLC (COL Sedge)  
Fort Detrick, Frederick  
MD 21701

Directorate  
of Training Development  
Bldg 502  
Fort Rucker, AL 36362

Chief  
Human Engineering Laboratory  
Field Unit  
Fort Rucker, AL 36362

Commander  
U.S. Army Aviation Center  
and Fort Rucker  
ATTN: ATZQ-T-ATL  
Fort Rucker, AL 36362

President  
U.S. Army Aviation Board  
Cairns AAF  
Fort Rucker, AL 36362